

# Microporous Polymeric Sorbent Technology for Post-Combustion CO<sub>2</sub> Capture

## primary project goal

The National Energy Technology Laboratory's Research and Innovation Center (NETL-RIC) is developing new, microporous polymeric (m-poly) sorbent technology with a demonstrated carbon dioxide (CO<sub>2</sub>) uptake capacity of 10 wt% and a selectivity of greater than 500 under a "simulated gas" environment for natural gas flue gas (NGFG). The most promising m-poly sorbents are to be integrated into a prototype modular system for long-term field testing (such as at the National Carbon Capture Center [NCCC]) under actual post-combustion flue gas.

## technical goals

- Identify a sorbent material with a potential of achieving a CO<sub>2</sub> uptake property of 7 wt% and a CO<sub>2</sub>/Nitrogen (N<sub>2</sub>) selectivity of 500. Evaluate materials under NGFG environments.
- Demonstrate the sorbent material in fiber form with a potential of achieving a CO<sub>2</sub> uptake property of 7 wt% and a CO<sub>2</sub> selectivity of 500. Evaluate the fiber materials under neat environments.
- Test a sorbent prototype under simulated or actual NGFG.
- Perform a techno-economic analysis (TEA) with experimental data to calculate the cost of achieving 95% capture efficiency (conducted by Strategic Systems Analysis and Engineering [SSAE] team).

## technical content

The selective removal of CO<sub>2</sub> from dilute, mixed gas streams at the scales associated with centralized power generation represents a significant challenge. Adding to this challenge is the need to rapidly develop and deploy a separation technology that delivers a viable option in the next few years with the delivered technology also having minimal impact on the delivered cost of electricity (COE) to the customer. Sorbent materials have been studied intensively in recent years for CO<sub>2</sub> capture. Inorganic sorbents, such as aminated silica and metal organic frameworks (MOFs), showed significant CO<sub>2</sub> capture performance. However, chemical stability, amine leaching, high regeneration temperature, slow sorption kinetics, and poor cyclability have been major drawbacks for these sorbents. On the other hand, polymeric sorbents, such as porous polymeric networks (PPNs) and benzimidazole linked polymers (BILPs), have been developed with high chemical stability and fast adsorption/desorption cycles. In general, porous polymers suffer from use of costly monomers/reactants, harsh synthesis conditions, and lower CO<sub>2</sub> capture capacity compared to their inorganic counterparts.

The removal of CO<sub>2</sub> from natural gas combined cycle (NGCC), as compared to coal-derived flue gas (pulverized coal), can be considered even more challenging. Carbon dioxide is present at lower levels (~4 vol% versus >12 vol%), representing less partial pressure driving force available for separation. Oxygen (O<sub>2</sub>) is significantly higher (~12 vol% versus 3 vol%), necessitating that the sorbent

### program area:

Point Source Carbon Capture

### ending scale:

Laboratory Scale

### application:

Post-Combustion Power Generation PSC

### key technology:

Sorbents

### project focus:

Shapeable Microporous Polymeric Sorbent

### participant:

National Energy Technology Laboratory—Research and Innovation Center

### project number:

FWP-1022402 (Task 17)

### predecessor project:

2020 Carbon Capture FWP

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possesses oxidative stability, a valid concern for amine-based materials. Moisture is lower for NGCC flue gas (~8 vol%) versus pulverized coal flue gas (~14 vol%), but can still include the difficulty of competitive adsorption of H<sub>2</sub>O being favored over CO<sub>2</sub>. There is a need for high CO<sub>2</sub> capacity sorbents that are chemically stable, inexpensive, and have a simple synthesis procedure.

Over the past several years, NETL has provided the foundational knowledge and technology progress that can overcome the challenges associated with the maturation of polymer-based sorbent technology. For example, NETL has developed BILPs demonstrating the highest CO<sub>2</sub> uptake and CO<sub>2</sub>/N<sub>2</sub> selectivity of all other PBIs reported to date (Figure 1). Low-temperature CO<sub>2</sub> regeneration, fast kinetics, and high chemical stability all combine to make this sorbent a promising candidate for carbon capture (Figure 1). The team recently developed a soluble m-poly functionalized with carboxylic acid groups. Functionalized polymers were impregnated with alkyl amines that formed a stable sorbent. These polymers showed high CO<sub>2</sub> uptake and CO<sub>2</sub>/N<sub>2</sub> selectivity, which is more than four times higher compared to similar sorbents. Sorbents tested under humid conditions showed chemical stability and the CO<sub>2</sub> uptake performance remained intact after several cycles. Moreover, these sorbents were able to be regenerated at 85°C.

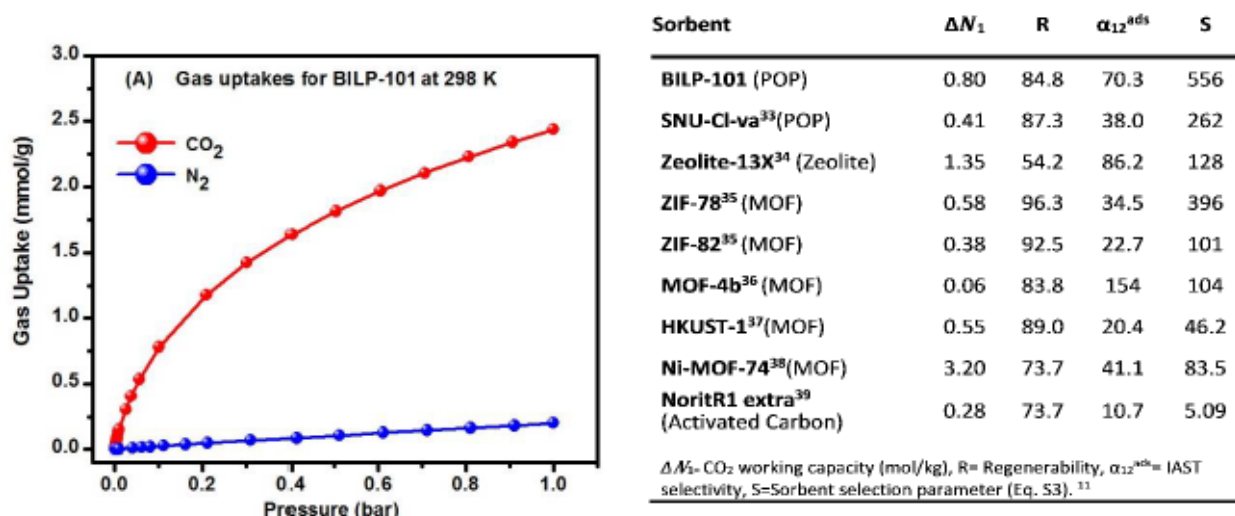


Figure 1: CO<sub>2</sub> and N<sub>2</sub> adsorption isotherm of the BILP sorbent and the list of top-performing sorbents for flue gas (CO<sub>2</sub>/N<sub>2</sub>:10/90) separation using vacuum swing adsorption at 298K, P<sub>ads</sub>=1 bar, and P<sub>des</sub>=0.1 bar.

In the first phase, several proposed polymeric sorbents were developed. Specifically, the sorbent series PIM-1-AO-DETA (Figure 2) showed high CO<sub>2</sub> uptake capacity (Figure 3) and CO<sub>2</sub>/N<sub>2</sub> selectivity, exceeding the 7 wt% CO<sub>2</sub> uptake milestones of the first year. Carbon dioxide uptake capacity of sorbents remains intact in humid conditions after several regeneration cycles (Figure 4). As-synthesized sorbents were characterized and scaled up to be processed into fibers in the second year.

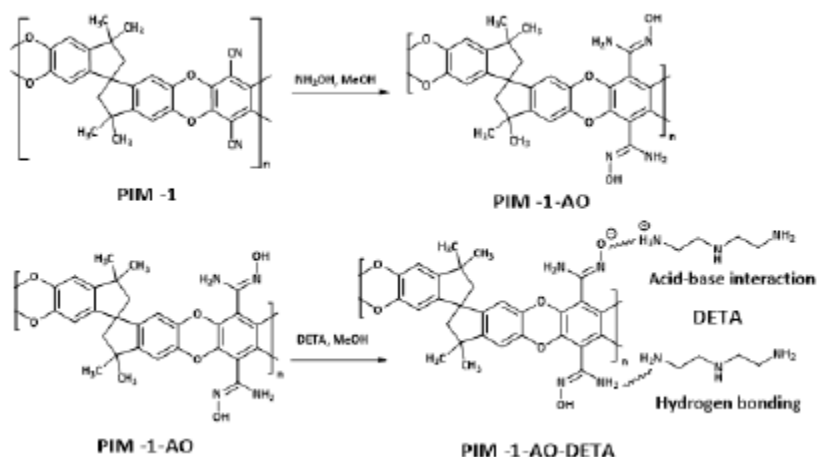


Figure 2: Reaction scheme and preparation of PIM-1-AO-DETA sorbent.

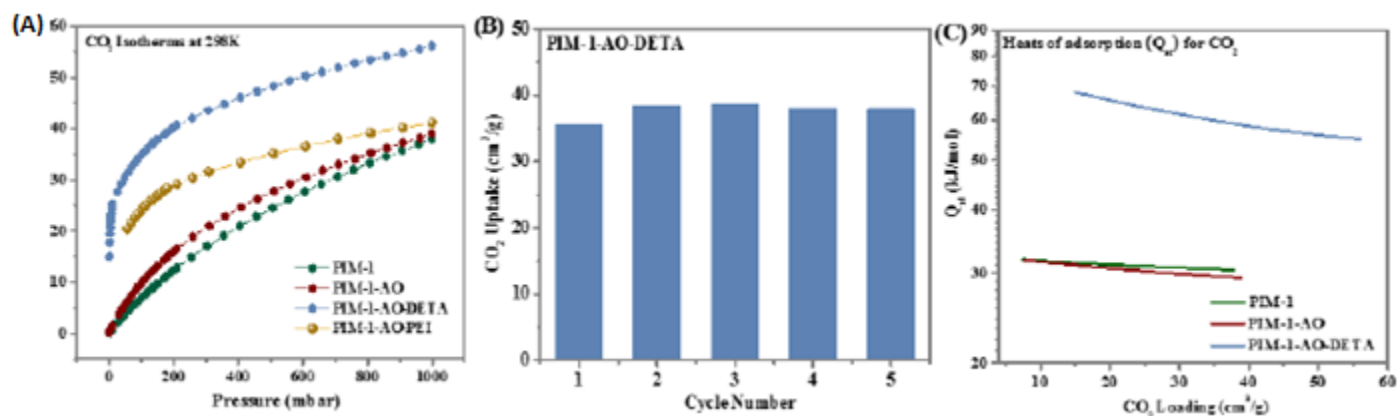


Figure 3: (A) CO<sub>2</sub> uptake isotherm of the discovered sorbent (PIM-1-AO-DETA) in comparison with neat PIM-1, functionalized (PIM-1-AO), and PEI impregnated PIM-1 (PIM-1-PEI). (B) CO<sub>2</sub> cyclability of PIM-1-AO-DETA (regenerated only at 80°C). (C) Heat of adsorption for CO<sub>2</sub> for the sorbents.

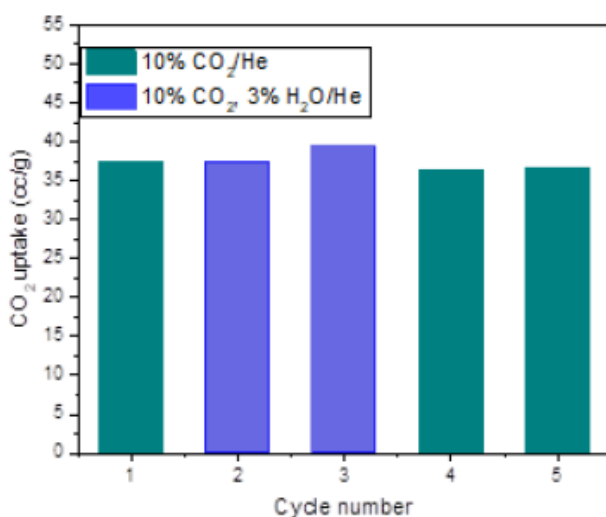


Figure 4: Preliminary CO<sub>2</sub> uptake performance of NETL's high-performance m-poly-1 tested in packed-bed reactor with gas breakthrough analysis under dry and humid conditions.

Continued work is being directed toward the development of new m-poly sorbents. The major advantage of m-poly over other porous materials, such as MOFs and zeolites, is very high chemical stability because of the strong covalent bond linking the polymer backbone. Unlike previous work with BILPs, these sorbents are being structured from contorted one-dimensional monomers, which provide sorbent solubility in common solvents. In the case of other sorbents, such as BILPs, MOFs, silica, and zeolites, they need to be processed with other additives, which usually causes a large decrease in their CO<sub>2</sub> uptake capacity. On the other hand, the proposed m-poly sorbents can be processed into desired sorbent shapes such as pellets, beads, fibers, etc., depending on the reactor design configuration envisioned for the capture process.

**TABLE 1: SORBENT PROCESS PARAMETERS**

| <b>Sorbent</b>                                                     | <b>Units</b>                   | <b>Current R&amp;D Value</b>      | <b>Target R&amp;D Value</b> |
|--------------------------------------------------------------------|--------------------------------|-----------------------------------|-----------------------------|
| True Density @ STP                                                 | kg/m <sup>3</sup>              | —                                 | —                           |
| Bulk Density                                                       | kg/m <sup>3</sup>              | 1.1                               | —                           |
| Average Particle Diameter                                          | mm                             | 1                                 | —                           |
| Particle Void Fraction                                             | m <sup>3</sup> /m <sup>3</sup> | —                                 | —                           |
| Packing Density                                                    | m <sup>2</sup> /m <sup>3</sup> | —                                 | —                           |
| Solid Heat Capacity @ STP                                          | kJ/kg-K                        | —                                 | —                           |
| Crush Strength                                                     | kg <sub>f</sub>                | —                                 | —                           |
| Manufacturing Cost for Sorbent                                     | \$/kg                          | —                                 | —                           |
| <b>Adsorption</b>                                                  |                                |                                   |                             |
| Pressure                                                           | bar                            | 0.1                               | —                           |
| Temperature                                                        | °C                             | 25                                | —                           |
| Equilibrium Loading                                                | g mol CO <sub>2</sub> /kg      | 2.1                               | —                           |
| Heat of Adsorption                                                 | kJ/mol CO <sub>2</sub>         | 47                                | —                           |
| <b>Desorption</b>                                                  |                                |                                   |                             |
| Pressure                                                           | bar                            | 1                                 | —                           |
| Temperature                                                        | °C                             | 75                                | —                           |
| Equilibrium CO <sub>2</sub> Loading                                | g mol CO <sub>2</sub> /kg      | 0.1                               | —                           |
| Heat of Desorption                                                 | kJ/mol CO <sub>2</sub>         | —                                 | —                           |
| <b>Proposed Module Design</b>                                      |                                | <i>(for equipment developers)</i> |                             |
| Flow Arrangement/Operation                                         | —                              | —                                 | —                           |
| Flue Gas Flowrate                                                  | kg/hr                          | —                                 | —                           |
| CO <sub>2</sub> Recovery, Purity, and Pressure                     | % / % / bar                    | —                                 | —                           |
| Adsorber Pressure Drop                                             | bar                            | —                                 | —                           |
| Estimated Adsorber/Stripper Cost of Manufacturing and Installation | $\frac{\$}{\text{kg/hr}}$      | —                                 | —                           |

**Definitions:**

**STP** – Standard Temperature and Pressure (15°C, 1 atm).

**Sorbent** – Adsorbate-free (i.e., CO<sub>2</sub>-free) and dry material as used in adsorption/desorption cycle.

**Manufacturing Cost for Sorbent** – “Current” is market price of material, if applicable; “Target” is estimated manufacturing cost for new materials, or the estimated cost of bulk manufacturing for existing materials.

**Adsorption** – The conditions of interest for adsorption are those that prevail at maximum sorbent loading, which typically occurs at the bottom of the adsorption column. These may be assumed to be 1 atm total flue-gas pressure (corresponding to a CO<sub>2</sub> partial pressure of 0.13 bar) and 40°C; however, measured data at other conditions are preferable to estimated data.

**Desorption** – The conditions of interest for desorption are those that prevail at minimum sorbent loading, which typically occurs at the bottom of the desorption column. Operating pressure and temperature for the desorber/stripper are process-dependent. Measured data at other conditions are preferable to estimated data.

**Pressure** – The pressure of CO<sub>2</sub> in equilibrium with the sorbent. If the vapor phase is pure CO<sub>2</sub>, this is the total pressure; if it is a mixture of gases, this is the partial pressure of CO<sub>2</sub>. Note that for a typical pulverized coal power plant, the total pressure of the flue gas is about 1 atm and the concentration of CO<sub>2</sub> is about 13.2%. Therefore, the partial pressure of CO<sub>2</sub> is roughly 0.132 atm or 0.130 bar.

**Packing Density** – Ratio of the active sorbent area to the bulk sorbent volume.

**Loading** – The basis for CO<sub>2</sub> loadings is mass of dry, adsorbate-free sorbent.

**Flow Arrangement/Operation** – Gas-solid module designs include fixed, fluidized, and moving bed, which result in either *continuous*, *cyclic*, or *semi-regenerative* operation.

**Estimated Cost** – Basis is kg/hr of CO<sub>2</sub> in CO<sub>2</sub>-rich product gas; assuming targets are met.

**Flue Gas Assumptions** – Unless noted, flue gas pressure, temperature, and composition leaving the flue gas desulfurization (FGD) unit (wet basis) should be assumed as:

| Pressure  | Temperature | Composition     |                  |                |                |      |                 |                 |
|-----------|-------------|-----------------|------------------|----------------|----------------|------|-----------------|-----------------|
|           |             |                 |                  | vol%           |                |      |                 | ppmv            |
| 14.7 psia | 135°F       | CO <sub>2</sub> | H <sub>2</sub> O | N <sub>2</sub> | O <sub>2</sub> | Ar   | SO <sub>x</sub> | NO <sub>x</sub> |
|           |             | 13.17           | 17.25            | 66.44          | 2.34           | 0.80 | 42              | 74              |

### Other Parameter Descriptions:

**Chemical/Physical Sorbent Mechanism** – Chemical structure of the sorbent consist of porous polymer with amidoxime and alkylamines functionalities.

**Sorbent Contaminant Resistance** – Sorbent is stable through humidity, sulfur oxide (SO<sub>x</sub>), and nitrogen oxide (NO<sub>x</sub>).

**Sorbent Attrition and Thermal/Hydrothermal Stability** – 200°C.

### technology advantages

- M-poly sorbent technology has small footprint, simplicity of device and process, ease of operation, modularity, and low parasitic energy requirements through low-temperature desorption (<85°C) to remove all adsorbed gases.
- The m-poly sorbent has high surface area, permanent microporosity, functionable structure, uniform pore size distribution, and high chemical and thermal stability, helping to address the challenges facing carbon capture from centralized point sources.
- Carbon dioxide uptake capacity of sorbents remains intact in humid conditions after several regeneration cycles.
- In contrast to other sorbents, soluble m-poly can be dissolved in common solvents and processed into the desired shape without any other material.

### R&D challenges

- There is a lack of polymer functionalization study and a lack of a detailed processability study to transfer technology to market.

### available reports/technical papers

Ali K. Sekizkardes, Sonia Hammache, James S. Hoffman, Polymers of Intrinsic Microporosity Chemical Sorbents Utilizing Primary Amine Appendage Through Acid–Base and Hydrogen-Bonding Interactions, David Hopkinson, ACS Appl. Mater. Interfaces 2019, 11, 34, 30987–30991, <https://doi.org/10.1021/acsami.9b09856>.

D. Hopkinson, A.K. Sekizkardes, Polymer for carbon dioxide capture and separation, U.S. Department of Energy, USA Patent no 10,323,125. 2019, pp. 22 <https://www.osti.gov/servlets/purl/1568476>.

A. Miles, W.C. Wilfong, D. Hopkinson, A.K. Sekizkardes, Alkylamine Incorporation in Amidoxime Functionalized Polymers of Intrinsic Microporosity for Gas Capture and Separation, Energy Technol. (Weinheim, Ger.), 8 (2020) 2000419. <https://doi.org/10.1002/ente.202000419>.

A.K. Sekizkardes, V.A. Kusuma, J.T. Culp, P. Muldoon, J. Hoffman, D. Hopkinson, Single polymer sorbent fibers for high performance and rapid direct air capture, ChemRxiv, (2022) 1-4. <https://doi.org/10.26434/chemrxiv-2022-jgpqv>.